Table A． 1 －Conversion of hardness－to－hardness or hardness－to－tensile－strength values for unalloyed and low alloy steels and cast steel
碳钢，低合金钢和铸钢的硬度－硬度，硬度－抗拉强度换算值

| Tensile | Vickers | Brinell | Rockwell hardness |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MPa | HV10 | HB ${ }^{\text {a }}$ | HRB | HRF | HRC | HRA | HRD | HR15N | HR30N | HR45N |
| 255 | 80 | 76，0 |  |  |  |  |  |  |  |  |
| 270 | 85 | 80，7 | 41，0 |  |  |  |  |  |  |  |
| 285 | 90 | 85，5 | 48，0 | 82，6 |  |  |  |  |  |  |
| 305 | 95 | 90，2 | 52，0 |  |  |  |  |  |  |  |
| 320 | 100 | 95，0 | 56，2 | ：：8\％ |  |  |  |  |  |  |
| 335 | 105 | 99，8 |  | ：$: 7:$ |  |  |  |  |  |  |
|  |  | 105 |  | $\because \because$ |  |  |  |  |  |  |
| 350 | 110 | 105 | 62.3 | 90，5： |  |  |  |  |  |  |
| 370 | 115 | 109 | ：$: 8:$ |  |  |  |  |  |  |  |
| 385 | 120 | 114 | ¢\％\％\％ | 93，6 |  |  |  |  |  |  |
| 400 | 125 | 119 | ！ |  |  |  |  |  |  |  |
| 415 | 130 | 124 | 71，2： | ：90，90 |  |  |  |  |  |  |
| 430 | 135 |  | ．： | ：$:$ |  |  |  |  |  |  |
| 430 | 135 | 128：0： | ：$: ~:$ |  |  | ：$:$ |  |  |  |  |
| 450 | 140 | ： $7338:$ | ： 5 | $\because 99,0$ |  | ： |  |  |  |  |
| 465 | 145 | $\because: \because 9{ }^{\circ} 8^{\prime \prime}$ | ：$: 8: 8$ |  |  | ： |  |  |  |  |
| 480 | 150 | $\because: \% 43$ | \％ | 101，4 |  |  |  |  |  |  |
| 495 | 155： | $:: 147$ | $\because: \because:$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 510 | 160 | $::$ ：\＄5\％ | $84 \%$ | 103，6 |  |  |  |  |  |  |
| 530 | 165 |  |  |  |  |  |  |  |  |  |
| 545 | 170 | 162 | $\dot{8} 50$ | 105： |  |  |  |  |  |  |
| 560 | 175 | 166 | ：$\because:$ | 1：$\because: 8$ |  | $\because \cdot$ | $\because: \because$ |  |  |  |
|  | 175 |  | ： | －：．：日： |  |  |  | ．．．： |  |  |
| 575 | 180 | 171 | 879 | ： 107072 |  |  |  |  |  |  |
| 595 | 185 | 176 |  | $\because: \%$ |  |  |  |  |  |  |
| 610 | 190 | 181 | 89，5 | $\because 108,7$ |  |  |  |  |  |  |
| 625 | 195 | 185 |  |  |  |  |  |  |  |  |
| 640 | 200 | 190 | 91，5 | 110，1 |  |  |  |  |  |  |
| 660 | 205 | 195 | 92，5 |  |  |  |  |  |  |  |
| 675 | 210 | 199 | 93，5 | 111，3 |  |  |  |  |  |  |
| 690 | 215 | 204 | 94，0 |  |  |  |  |  |  |  |
| 705 | 220 | 209 | 95，0 | 112，4 |  |  |  |  |  |  |
| 720 | 225 | 214 | 96，0 |  |  |  |  |  |  |  |
| a Brinell hardness values up to 450 HB were determined using a steel ball indenter，those above this value were determined with a hardmetal ball． |  |  |  |  |  |  |  |  |  |  |
| NOTE 1 Values in parentheses are those lying outside the defined range of the standard test method but which may used as estimates． |  |  |  |  |  |  |  |  |  |  |
| NOTE 2 The value of the tension test are not based on method A（10．3 Testing rate based on close－loop control at the rate of the extension）in ISO 6892－1：2009 |  |  |  |  |  |  |  |  |  |  |

Table A. 1 (continued)

| Tensile | Vickers | Brinell | Rockwell hardness |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MPa | HV10 | HB a | HRB | HRF | HRC | HRA | HRD | HR15N | HR30N | HR45N |
| 740 | 230 | 219 | 96,7 | 113,4 |  |  |  |  |  |  |
| 755 | 235 | 223 |  |  |  |  |  |  |  |  |
| 770 | 240 | 228 | 98,1 | 114,3 | 20,3 | 60,7 | 40,3 | 69,6 | 41,7 | 19,9 |
| 785 | 245 | 233 |  |  | 21,3 | 61,2 | 41,1 | 70,1 | 42,5 | 21,1 |
| 800 | 250 | 238 | 99,5 $\quad \therefore$ | . 115,1 | 22,2 | 61,6 | 41,7 | 70,6 | 43,4 | 22,2 |
| 820 | 255 | 242 | : | $\because: \%$ | 23,1 | 62,0 | 42,2 | 71,1 | 44,2 | 23,2 |
| 835 | 260 | 247 | 19019: | $\because: 8: 8:$ | 24,0 | 62,4 | 43,1 | 71,6 | 45,0 | 24,3 |
| 850 | 265 | 252 | : $\because: \because:$ | $\because \because: 8:$ | 24,8 | 62,7 | 43,7 | 72,1 | 45,7 | 25,2 |
| 865 | 270 | 257 | : $\because\left[\begin{array}{l}\text { (10) }\end{array}\right.$ | $\because:$ | 25,6 | 63,1 | 44,3 | 72,6 | 46,4 | 26,2 |
| 880 | 275 | 261 | $\because: \%$ |  | . $26.90 \%$ | $\therefore$. 63,5 | 44,9 | 73,0 | 47,2 | 27,1 |
| 900 | 280 | 266 | $\because(104)$ | :: | -270ำ: | $\because \because 68$ | 45,3 | 73,4 | 47,8 | 27,9 |
| 915 | 285 | 271 | : $: 8: 8:$ | : : : : : | :: 27,8 | $\because: 848^{2}$ | 46,0 | 73,8 | 48,4 | 28,7 |
| 930 | 290 | :279\% | (10) | : $: 8: 8$ | 28,5: | $\because \because 64,5$ | 46,5 | 74,2 | 49,0 | 29,5 |
| 950 | 295 | : $\because: 880$ | :8:8: |  | 2, ${ }^{\circ} \mathrm{O}$ | $\because 64,8$ | 47,1 | 74,6 | 49,7 | 30,4 |
| 965 | 300: | : |  |  | , | -65,2 | 47,5 | 74,9 | 50,2 | 31,1 |
| 995 |  | $\because 295$ | : $: 8: 8: 8$ |  | $\because: 31,0$ | 65,8 | 48,4 | 75,6 | 51,3 | 32,5 |
| 1030 | 32̇90: | ?: 304 | : $: 8: 8$ |  | 32,2 | . $66 \% 4$ | 49,4 | 76,2: | 52,3 | 33,9 |
| 1060 | $330: 8:$ | : $\because: 8$ : ${ }^{\text {aq4 }}$ | : $\because: 8: 8$ | $\therefore \quad \therefore$ | 33,3 | . 0.0 | 50,2 | : 76.80 | 53,6 | 35,2 |
| 1095 | 340 | : $\because: 8: 8$ |  | : $\because: 8:$ | 34,4 | : $: 8: 8$ | 51,1 | - | 54,4 | 36,5 |
| 1125 | 350 | 333 |  | $\because: 8: 8$ | 35,5 | $\because 68,1$ | 51,9 | 7989 | 55,4 | 37,8 |
| 1155 | 360 | 342 | : $\because:$ | : $: 8:$ | 36,6 | 68,7 | - 52,8 | $\because: 78,6^{\circ}$ | 56,4 | 39,1 |
| 1190 | 370 | 352 |  | $\because \cdot$ | 37,7 | 69,2 | 53,6 | 79,2 | 57,4 | 40,4 |
| 1220 | 380 | 361 |  |  | 38,8 | 69,8 | 54,4 | 79,8 | 58,4 | 41,7 |
| 1255 | 390 | 371 |  |  | 39,8 | 70,3 | 55,3 | 80,3 | 59,3 | 42,9 |
| 1290 | 400 | 380 |  |  | 40,8 | 70,8 | 56,0 | 80,8 | 60,2 | 44,1 |
| 1320 | 410 | 390 |  |  | 41,8 | 71,4 | 56,8 | 81,4 | 61,1 | 45,3 |
| 1350 | 420 | 399 |  |  | 42,7 | 71,8 | 57,5 | 81,8 | 61,9 | 46,4 |
| 1385 | 430 | 409 |  |  | 43,6 | 72,3 | 58,2 | 82,3 | 62,7 | 47,4 |
| 1420 | 440 | 418 |  |  | 44,5 | 72,8 | 58,8 | 82,8 | 63,5 | 48,4 |
| 1455 | 450 | 428 |  |  | 45,3 | 73,3 | 59,4 | 83,2 | 64,3 | 49,4 |

a Brinell hardness values up to 450 HB were determined using a steel ball indenter, those above this value were determined with a hardmetal ball.
NOTE 1 Values in parentheses are those lying outside the defined range of the standard test method but which may used as estimates.
NOTE 2 The value of the tension test are not based on method A (10.3 Testing rate based on close-loop control at the rate of the extension) in ISO 6892-1:2009

Table A. 1 (continued)

| Tensile | Vickers | Brinell | Rockwell hardness |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MPa | HV10 | HB a | HRB | HRF | HRC | HRA | HRD | HR15N | HR30N | HR45N |
| 1485 | 460 | 437 |  |  | 46,1 | 73,6 | 60,1 | 83,6 | 64,9 | 50,4 |
| 1520 | 470 | 447 |  |  | 46,9 | 74,1 | 60,7 | 83,9 | 65,7 | 51,3 |
| 1555 | 480 | 456 |  |  | 47,7 | 74,5 | 61,3 | 84,3 | 66,4 | 52,2 |
| 1595 | 490 | 466 |  |  | 48,4 | 74,9 | 61,6 | 84,7 | 67,1 | 53,1 |
| 1630 | 500 | 475 |  |  | 49,1 | 75,3 | 62,2 | 85,0 | 67,7 | 53,9 |
| 1665 | 510 | 485 |  | $\because: \because:$ | 49,8 | 75,7 | 62,9 | 85,4 | 68,3 | 54,7 |
| 1700 | 520 | 494 |  |  | 50,5 | 76,1 | 63,5 | 85,7 | 69,0 | 55,6 |
| 1740 | 530 | 504 |  |  | 51,1 | 76,4 | 63,9 | 86,0 | 69,5 | 56,2 |
| 1775 | 540 | 513 | : $:$ |  | 51,7 | 76,7 | 64,4 | 86,3 | 70,0 | 57,0 |
| 1810 | 550 | 523 | : $::$ |  | 52:3: | :77,0 | 64,8 | 86,6 | 70,5 | 57,8 |
| 1845 | 560 | 532 |  |  | 53,0: | :7\% | 65,4 | 86,9 | 71,2 | 58,6 |
| 1880 | 570 | 542 |  |  | 5j3 6 | : 77 | 65,8 | 87,2 | 71,7 | 59,3 |
| 1920 | 580 | $5559: 8$ |  | : | 54,1 | :780 | 66,2 | 87,5 | 72,1 | 59,9 |
| 1955 | 590 | -:58\% |  |  | 54,7, | :78,4 | 66,7 | 87,8 | 72,7 | 60,5 |
| 1995 | 600 | : $:: 75 \%$ |  |  | 55, ${ }^{\circ}$ | :78,6 | 67,0 | 88,0 | 73,2 | 61,2 |
| 2030 | 610 | $\because: 580$ | : $: 8:$ |  | \% 555, ${ }^{\circ}$ | 78,9 | 67,5 | 88,2 | 73,7 | 61,7 |
| 2070 | 620 : $: ~:$ | $\because: 8589$ | : $: 8: 8$ |  | 56,3 | 79,6: | 67,9 | 88,5:• | 74,2 | 62,4 |
| 2105 | 630 | : $: ~: 8$ :599\% |  |  | 56,8 | 79:30 | 68,3 | 88.80 | 74,6 | 63,0 |
| 2145 | 640 | $\because 808{ }^{\circ}$ |  |  | 57,3 | :79\%\% | 68,7 | . $8900{ }^{\circ}$ | 75,1 | 63,5 |
| 2180 | 650 | 618 |  |  | 57,8 | 89\%\% | :89,0 | -899\%: | 75,5 | 64,1 |
|  | 660 |  | : $: ~:$ | : $: 8: 8:$ | 58,3 | 80,3 | 69,4 | $89,5 \cdot$ | - 75,9 | 64,7 |
|  | 670 |  |  | :8: | 58,8 | 80,6 | 69,8 | 89,7 | 76,4 | 65,3 |
|  | 680 |  |  | : | 59,2 | 80,8 | 70,1 | 89,8 | 76,8 | 65,7 |
|  | 690 |  |  |  | 59,7 | 81,1 | 70,5 | 90,1 | 77,2 | 66,2 |
|  | 700 |  |  |  | 60,1 | 81,3 | 70,8 | 90,3 | 77,6 | 66,7 |
|  | 720 |  |  |  | 61,0 | 81,8 | 71,5 | 90,7 | 78,4 | 67,7 |
|  | 740 |  |  |  | 61,8 | 82,2 | 72,1 | 91,0 | 79,1 | 68,6 |
|  | 760 |  |  |  | 62,5 | 82,6 | 72,6 | 91,2 | 79,7 | 69,4 |
|  | 780 |  |  |  | 63,3 | 83,0 | 73,3 | 91,5 | 80,4 | 70,2 |
|  | 800 |  |  |  | 64,0 | 83,4 | 73,8 | 91,8 | 81,1 | 71,0 |

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Table A． 1 （continued）

| Tensile strength | Vickers hardness | Brinell hardness | ：Rockwell hardness |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MPa | HV10 | HB a | HRB |  | HRC | HRA | HRD | HR15N | HR30N | HR45N |
|  | 820 |  |  | ！ | 64：4\％： | 83，8 | 74，3 | 92，1 | 81，7 | 71，8 |
|  | 840 |  |  | ：＇${ }^{\text {a }}$ | 65，3： | 84，1 | 74，8 | 92，3 | 82，2 | 72，2 |
|  | 860 |  |  | : | 6品管: | 84，4 | 75，3 | 92，5 | 82，7 | 73，1 |
|  | 880 |  | 品 | \％ | 66，4 | 84，7． | 75，7 | 92，7 | 83，1 | 73，6 |
|  | 900 |  |  |  | 67,0,0: | 85，Q： | 76，1 | 92，9 | 83，6 | 74，2 |
|  | 920 |  |  | 品如 | 67，5： | \％85，3 3 ： | 76，5 | 93，0 | 84，0 | 74，8 |
|  | 940 |  |  | ：： | 68，0 | 85，6 | 76，9 | 93，2 | 84，4 | 75，4 |

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